## Q% m³/s **Electrical Power Generation - Forge Weir, Halton** 1 326.4 2 211.7 177.3 3 350.0 4 152.6 Flow m<sup>3</sup>/s 2.15 Q <sub>mear</sub> 5 136.2 Water to water head with increased river flow 2.1 6 124.9 2.05 7 113.7 300.0 8 106.5 1.95 9 99.3 10 1.9 92.8 1.85 11 86.4 250.0 12 81.7 1.8 M³/s 13 78.6 1.75 0 20 40 60 100 120 140 14 74.8 80 160 180 200 220 200.0 15 71.2 16 66.9 HLH Theodolite, mid outfall, calibration check. Original survey 2m slightly upstream of HLH 17 63.6 Segen 1Jun10 10.24m - 8.02m = 2.24m with 4.87m<sup>3</sup>/s 18 59.9 150.0 Flow Duration Curve - Caton 19 57.5 20 54.9 21 52.2 22 50.1 100.0 23 48.0 Turbine 1 Flow 24 45.8 25 44.1 26 42.5 50.0 Turbine 2 27 40.2 related limits 28 38.7 29 37.3 30 35.4 0.0 50 31 33.9 10 20 30 40 70 80 100 32 32.7 Reserve Flow Percent exceeded 33 31.5 34 30.3 CALCULATIONS FOR THE FIRST, FOLLOWED BY THE SECOND TURBINE 35 29.2 36 28.5 Hands off, reserve flow for fish passage 4.74 m<sup>3</sup>/s $Q_{90}$ 37 27.1 Water flow for turbines, up to 12.00 38 26.2 River flow utilisation, total 16.74 39 25.1 40 24.1 Turbine 1 100 kWe Nominal flow 5.96 m<sup>3</sup>/s at 2m head 41 23.4 Gross Head 2.1m 42 22.5 Nett head less an estimated 9% losses 1.911 6.24 m<sup>3</sup>/s 43 21.7 10.98 Total Q<sub>65</sub> 44 20.8 Variation with lost head, worst case. (Inset graph) 1.85m, 150m<sup>3</sup>/s river, Q<sub>4</sub> $6.74 \text{ m}^3/\text{s}$ and $Q_{63}$ 45 20.1 Compensated flow, worst case 11.48 M<sup>3</sup>/s total 46 19.4 Flow is available & hence not influential on MW-hr calculation 47 18.8 92.5% 48 18.2 49 17.6 Turbine runs at full power for 65% of the 8,760hrs pa 569.4 MW-hr pa 50 17.0 Part load running down to 25% of full power flow 1.49 m<sup>3</sup>/s cut off 51 16.5 6.23 Total or Q<sub>83</sub> 52 15.6 Apportioning the triangle area from the rectangle area 53 15.5 54 Rectangle 6.24 x 65 405.6 569.4 MW-hr pa 15.1 55 14.5 Triangle (83-65) x 6.24/2 56.16 78.84 MW-hr 56 648.2 MW-hr Cash flow calculation has used 14.1 57 13.7 Q% m<sup>3</sup>/s Worst case 94% mechanical to electrical 609.35 MW-hr Net 593.75 MW-hr nett 7.12 58 79 13.2 Shutdown period Q100 minus Q83 = 17% 62.05 days for planned maintenance 59 12.8 80 6.92 60 12.4 81 6.65 Repeat for the addition of a second turbine, assuming 100kWe - and see where the limitations are. 61 12.1 82 6.44 The reserve flow remains the same and the 12m<sup>3</sup>/s extraction becomes a limiting factor 62 11.7 83 6.2 Both 100kW turbines at full power requires 17.22 which is over the 16.74 allowance 63 11.4 84 5.98 Both will run at less than full power at 97% of 200kWe 194.4 kW 64 85 5.79 11.1 65 Alternatively, keep the first turbine at full power and the second turbine maximum flow is 5.76 m<sup>3</sup>/s 10.8 86 5.62 87 5.37 66 10.5 Equivalent river flow will thus be 16.73 Q<sub>50</sub> 67 10.2 88 5.18 The second turbine cut-off will be when the water availability falls below it's 1.49m<sup>3</sup>/s 12.47 Q<sub>60</sub> The areas of the additional rectangle and triangle are:-68 10.0 89 4.94 69 9.6 90 4.74 Rectangle 5.76 x 50 288 70 9.4 91 4.54 Triangle (60-50) x 5.76/2 28.8 444.7 MW-hr gross 71 4.28 9.1 92 Area units 316.8 72 8.8 93 3.89 Worst case 94% mechanical to electrical 418.1 MW-hr 73 8.5 94 3.68 There will also be some high river flow loss of head, not compensated - say 5% 397.15 MW-hr 74 95 8.3 3.46 Grant Total MW-hr pa Net 1006.5 The period of shutdown will be longer than turbine one, although in reality they will both share, shutdown time. 75 96 3.27 8.1 76 7.8 97 3.00 77 7.6 98 2.75 78 7.4 99 2.36